

**AMENDMENTS TO THE CLAIMS**

**This listing of claims will replace all prior versions and listings of claims in the application:**

**LISTING OF CLAIMS:**

1. (currently amended): A sintered ferrite body having a main composition comprising ~~63-80%~~ 68-75% by mol of  $\text{Fe}_2\text{O}_3$ , and ~~3-15~~ 12% by mol of ZnO, the balance being manganese oxide;  $R_{\text{cal}}$  determined from the  $\text{Fe}_2\text{O}_3$  content X (% by mol) by the formula (1) of  $R_{\text{cal}} = [200(X-50)]/(3X)$ , and the ratio R (%) of  $\text{Fe}^{2+}$  per the total amount of Fe in said sintered body meeting the condition of  $R_{\text{cal}} - 2.0 \leq R \leq R_{\text{cal}} + 0.3$ ; ~~and said sintered body having a density of 4.9 g/cm<sup>3</sup> or more; and said sintered ferrite body having a maximum magnetic flux density of 540 mT or more measured at 100°C in a magnetic field of 1000 A/m.~~
2. (canceled).
3. (previously presented): The sintered ferrite body according to claim 1, comprising 0.02-0.3% by weight (calculated as  $\text{CaCO}_3$ ) of Ca, and 0.003-0.015% by weight (calculated as  $\text{SiO}_2$ ) of Si, as sub-components, per 100% by weight of the main composition.
4. (previously presented): The sintered ferrite body according to claim 1, wherein said sintered ferrite body has volume resistivity of 0.1  $\Omega \cdot \text{m}$  or more.

5. (previously presented): The sintered ferrite body according to claim 1, wherein said sintered ferrite body has a minimum-core-loss temperature of 80°C-120°C.

6. (previously presented): An electronic part formed by winding a wire around a magnetic core comprising the sintered ferrite body recited in claim 1.

7. (currently amended): A method for producing a sintered ferrite body having a main composition comprising ~~63-80%~~ 68-75% by mol of  $\text{Fe}_2\text{O}_3$ , and ~~3-15~~ 12% by mol of ZnO, the balance being manganese oxide;  $R_{\text{cal}}$  determined from the  $\text{Fe}_2\text{O}_3$  content X (% by mol) by the formula (1) of  $R_{\text{cal}} = [200(X-50)]/(3X)$ , and the ratio R (%) of  $\text{Fe}^{2+}$  per the total amount of Fe in the sintered body meeting the condition of  $R_{\text{cal}} - 2.0 \leq R \leq R_{\text{cal}} + 0.3$ ; ~~and said sintered body having a density of 4.9 g/cm<sup>3</sup> or more; and said sintered ferrite body having a maximum magnetic flux density of 540 mT or more measured at 100°C in a magnetic field of 1000 A/m,~~ said method comprising a step of adding a binder to ferrite powder, a molding step, a binder-removing step and a sintering step, said ferrite powder having a spinelization ratio S of 10-60%; the amount V (% by weight) of said binder added being in a range of  $1.3 - 0.02S \leq V \leq 2.3 - 0.02S$ , assuming that the total amount of said ferrite powder and said binder is 100% by weight; the oxygen concentration in the atmosphere from said binder-removing step to the completion of said sintering step in a temperature range of 1150-1250°C being 0.1% or less by volume.

8. (original): The method for producing a sintered ferrite body according to claim 7, wherein said spinelization ratio of ferrite powder is 10-40%.

9. (previously presented): The method for producing a sintered ferrite body according to claim 7, wherein said ferrite powder has a specific surface area of 3000-7000 m<sup>2</sup>/kg.

10. (canceled).

11. (previously presented): The method for producing a sintered ferrite body according to claim 7, wherein 0.02-0.3% by weight (calculated as CaCO<sub>3</sub>) of Ca, and 0.003-0.015% by weight (calculated as SiO<sub>2</sub>) of Si are added as sub-components to 100% by weight of said main composition.

12. (canceled).

13. (previously presented): The sintered ferrite body according to claim 1, wherein said sintered ferrite body has a reduction ratio of a maximum magnetic flux density from 20°C to 100°C of 10% or less.

14. (canceled).

15. (canceled).